

BLACK LIQUOR CHAR REACTIVITY WITH CO₂ IN OXY-COMBUSTION CONDITIONS

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Research Objectives

Investigate Char Reactivity in CO/CO₂ Atmospheres:

- Study the influence of varying CO and CO₂ ratios on gasification rates and thermal conversion behavior of black liquor char.

Assess Impact of Pyrolysis Conditions:

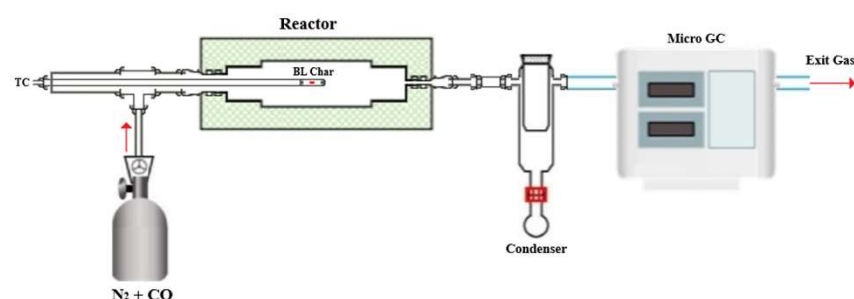
- Analyze how slow and fast pyrolysis affect char reactivity.

Development of a Kinetic model:

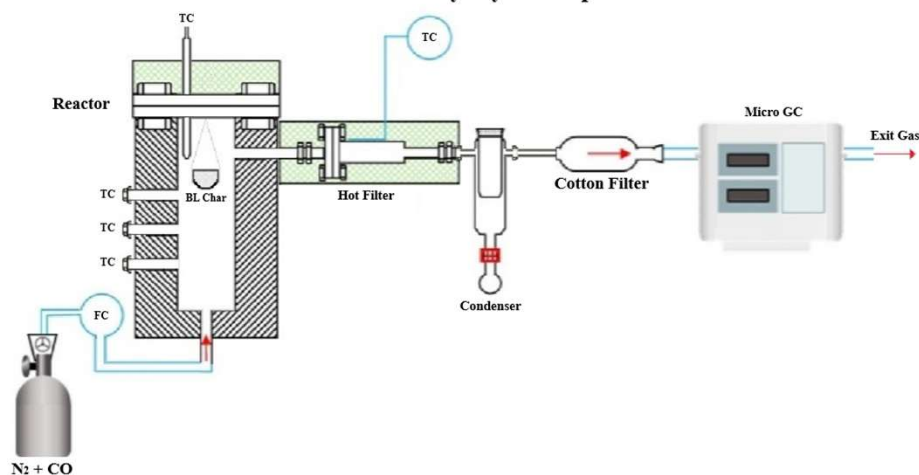
- Generate experimental data to be fed into a kinetic model to better understand the effects of the oxy-combustion conditions over the black liquor char.

Sample Preparation

Fast Pyrolysis Setup



Slow Pyrolysis Setup



Drying and Grinding of Black Liquor

- Black liquors were spread in thin layers and dried for 48 hours at 105°C, dried samples were finely ground and stored in sealed vials to avoid moisture uptake.

Char Production via Pyrolysis

- Pyrolysis was conducted using two heating regimes: slow and fast.
- Both processes used 90% N₂ and 10% CO as carrier gas.

Slow Pyrolysis Procedure

- Heated at 10°C/min to 900°C and held for 30 minutes.

Fast Pyrolysis Procedure

- Heated at 50°C/min to 900°C and held for 30 minutes.

Reactivity Experimental Setup



Fixed Bed Reactor Configuration

- Experiments conducted in a fixed bed ceramic reactor with 8 mm internal diameter.
- Reactor externally heated by an electric furnace.

Sample Feeding

- Approximately 25 mg of char loaded into the reactor.
- Char held in place by ceramic wool to ensure stable positioning.

Types of Experiments

Dynamic (IPL/IPR*)

- Li&Van Heiningen (5 – 15% CO)
- High CO₂ concentration (40 – 90% CO₂)

Isothermal (IPL/IPR*)

- Li&Van Heiningen (5 – 15% CO)
- High CO₂ concentration (40 – 90% CO₂)**

Dynamic-Isothermal (IPL/IPR*)

*IPL – Slow Pyrolysis Char

*IPR – Fast Pyrolysis Char

**Yet to be done

Dynamic Experiments Procedure

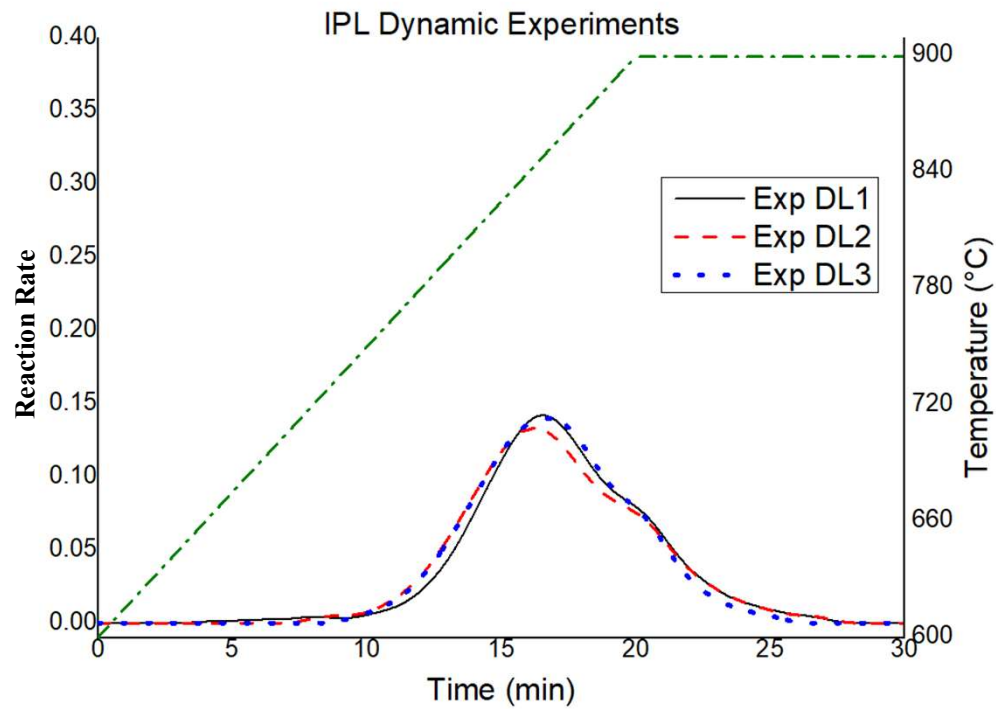
Temperature Range

- Final temperature preset to 900°C.

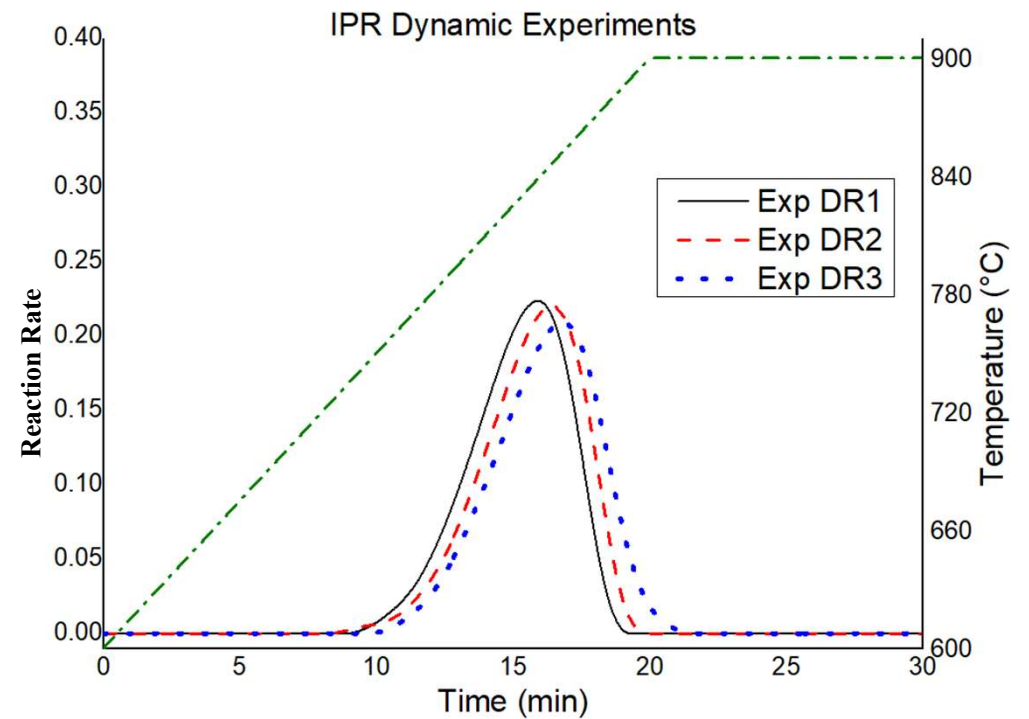
Gas Composition

- Initial gas: 90% N₂ and 10% CO.
- At 550°C, CO₂ introduced by partially replacing N₂.
- Final mixture adjusted progressively during the heating phase, reaching 5–20% CO₂ and 5–15% CO.

Dynamic Experiments – IPL/IPR

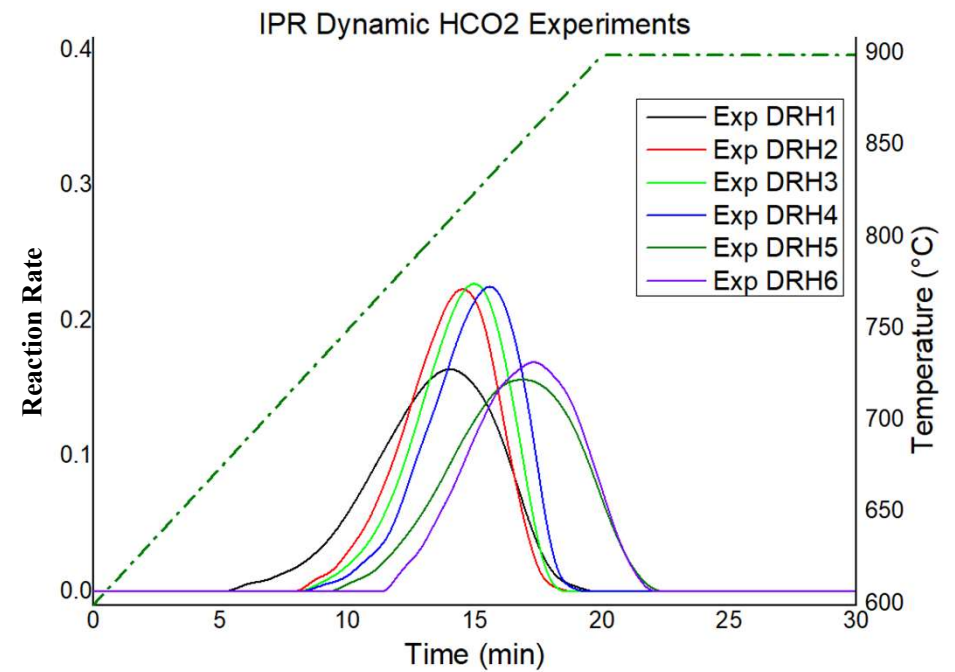
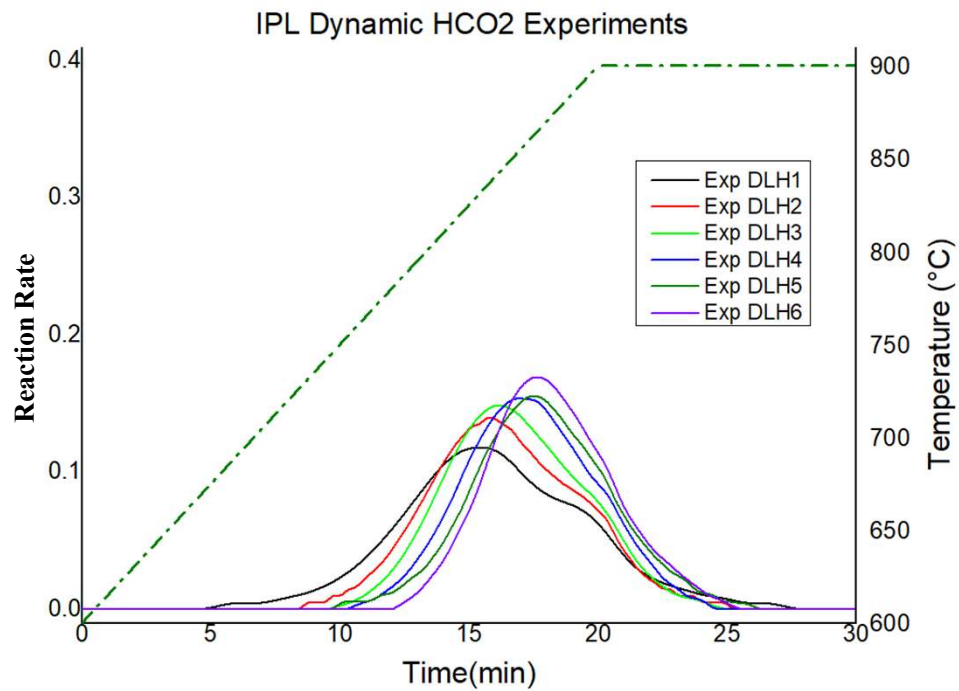


Exp DL1 – 10% CO + 20% CO₂
 Exp DL2 – 10% CO + 13% CO₂
 Exp DL3 – 10% CO + 5% CO₂



Exp DR1 – 10% CO + 20% CO₂
 Exp DR2 – 10% CO + 13% CO₂
 Exp DR3 – 10% CO + 5% CO₂

Dynamic High CO₂ Experiments – IPL/IPR



Exp DLH1/DRH1 – 10% CO + 90% CO₂
Exp DLH2/DRH2 – 20% CO + 80% CO₂

Exp DLH3/DRH3 – 30% CO + 70% CO₂
Exp DLH4/DRH4 – 40% CO + 60% CO₂

Exp DLH5/DRH5 – 50% CO + 50% CO₂
Exp DLH6/DRH6 – 60% CO + 40% CO₂

Isothermal Experiments Procedure

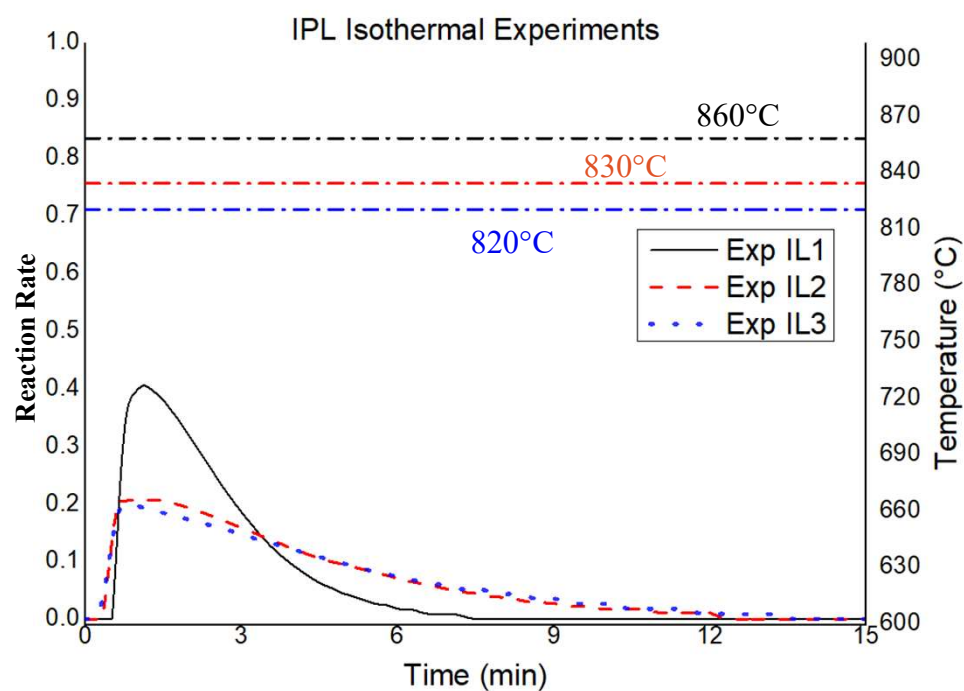
Temperature Range

- Experiments conducted at constant temperatures between 800°C and 900°C.

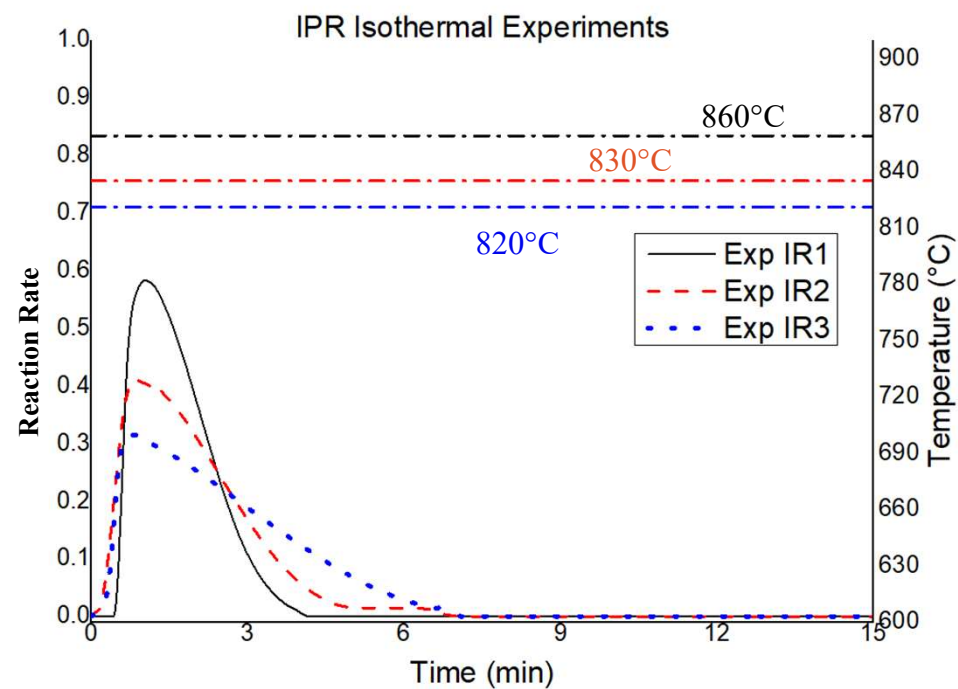
Gas Composition

- Initial gas: 90% N₂ and 10% CO.
- CO₂ introduced after a 20-minute isothermal hold by displacing an equivalent amount of N₂.
- Final mixture: 5–20% CO₂ and 5–15% CO, balanced with N₂.

Isothermal Experiments – IPL/IPR

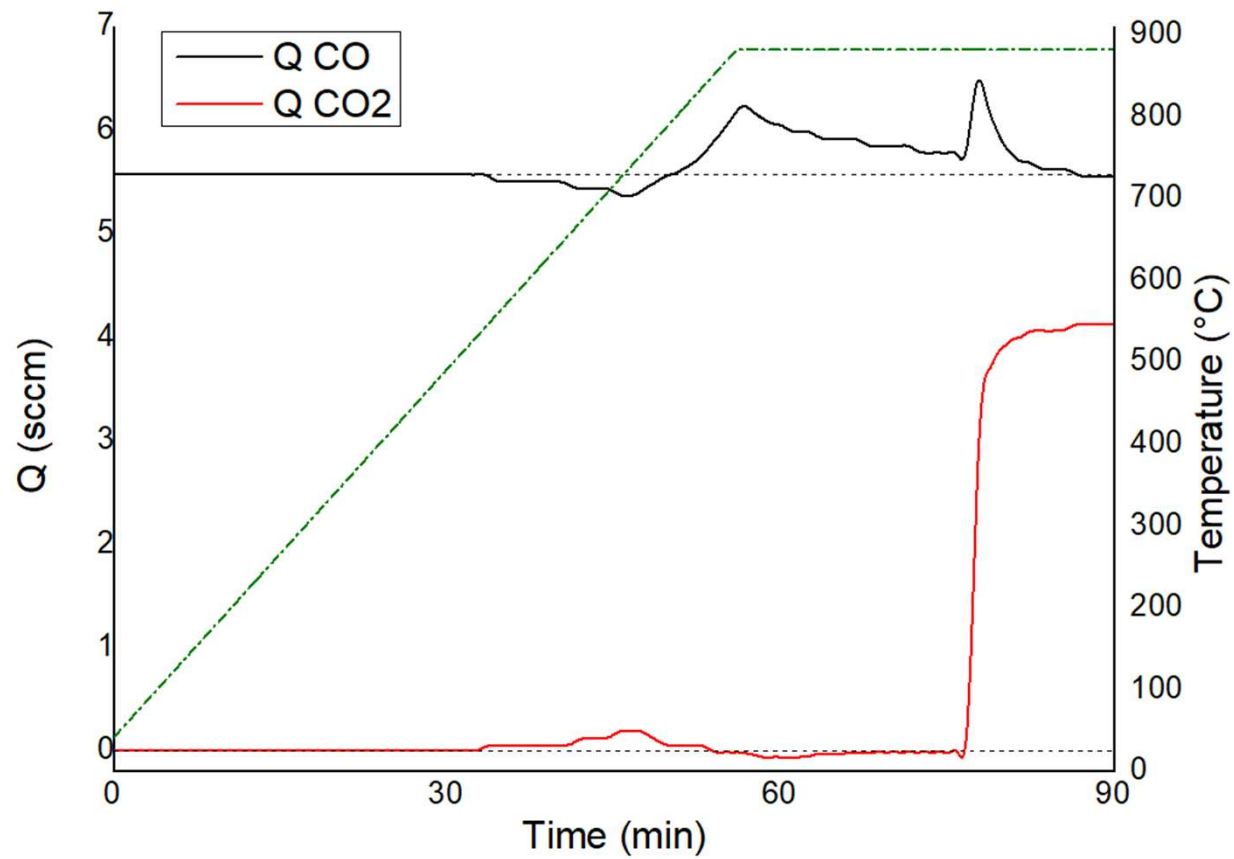


Exp IL1 – 9% CO + 12% CO₂
 Exp IL2 – 19% CO + 10% CO₂
 Exp IL3 – 13% CO + 8% CO₂

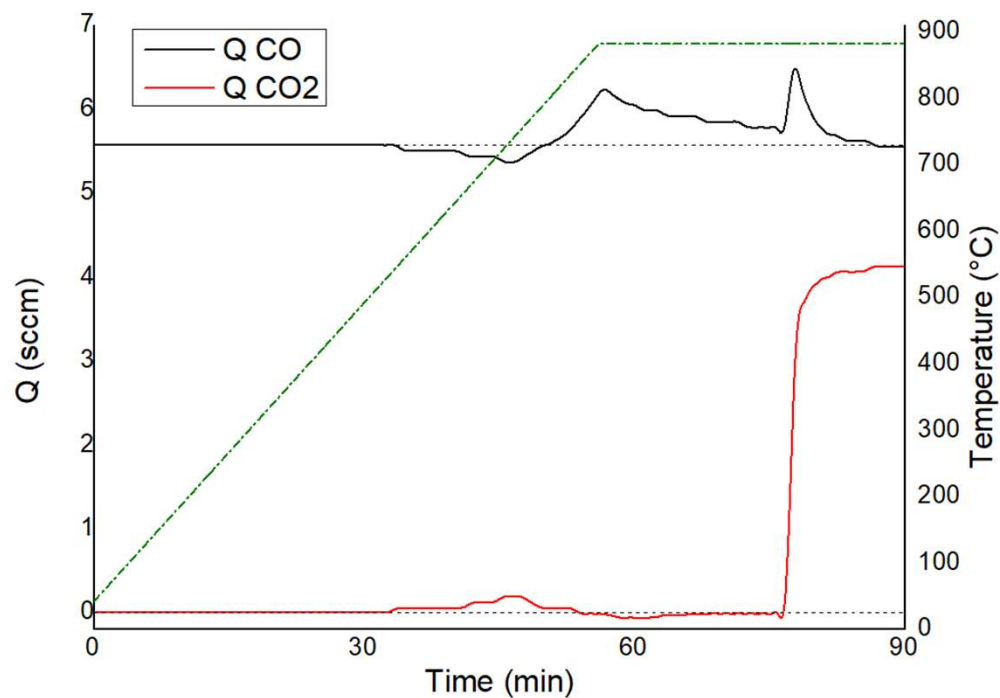


Exp IR1 – 9% CO + 12% CO₂
 Exp IR2 – 19% CO + 10% CO₂
 Exp IR3 – 13% CO + 8% CO₂

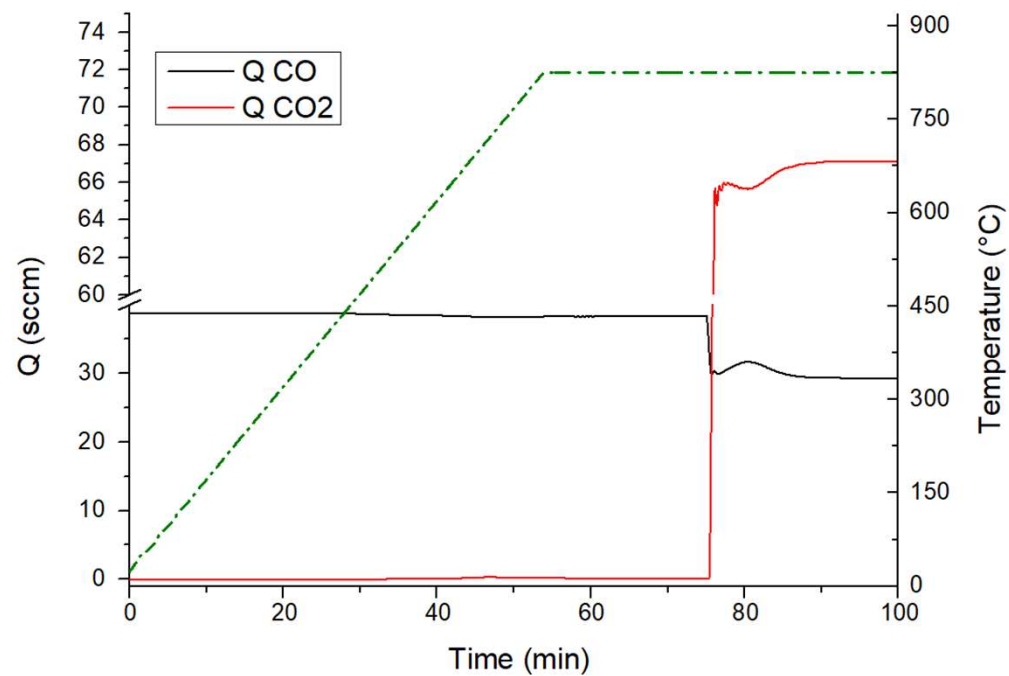
Isothermal Experiments – Char Decomposition



Char Decomposition Solution



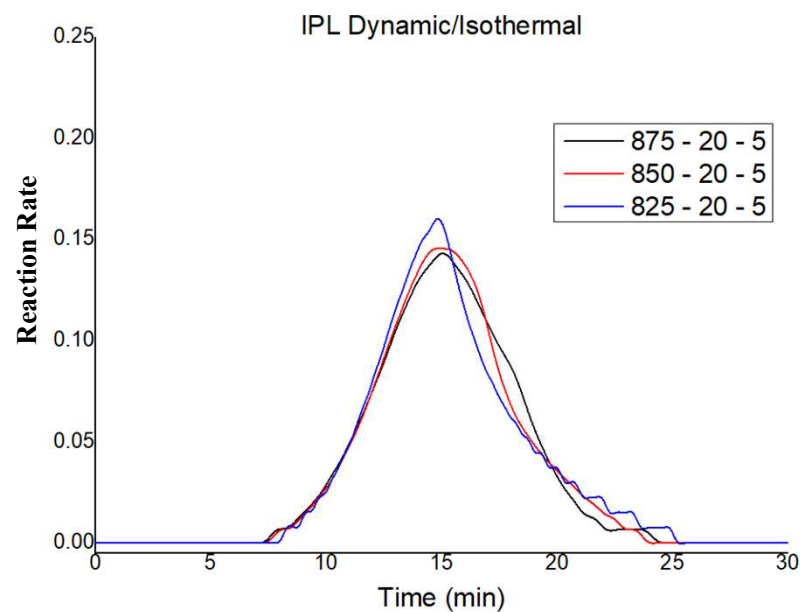
Area = 0.04459



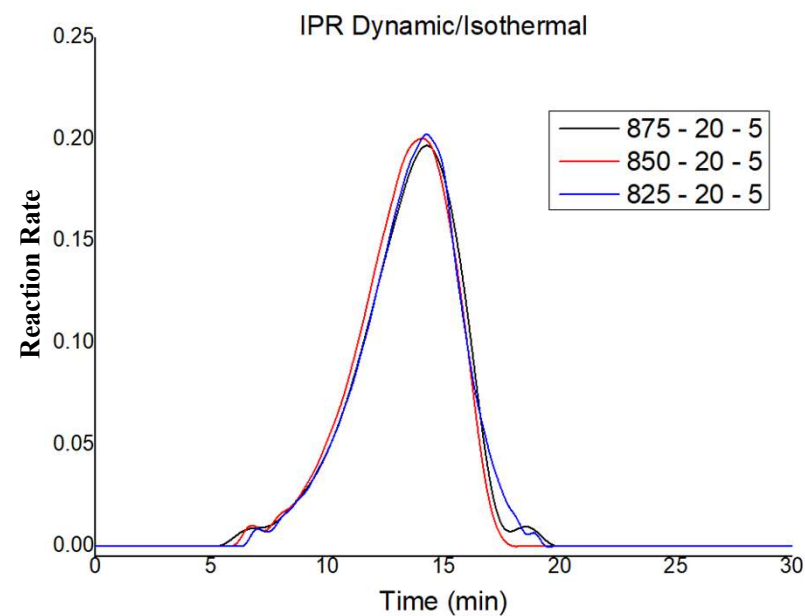
Area = 0.37594

Expected Area Range: $0,19 < \text{Area} < 0,38$ mmol of C gasified

Dynamic/Isothermal Experiments – IPL/IPR



Area 875°C = 0.21729
Area 850°C = 0.21273
Area 825°C = 0.18557



Area 875°C = 0.17953
Area 850°C = 0.17773
Area 825°C = 0.21800

Expected Area Range: $0,19 < \text{Area} < 0,38$ mmol of C gasified

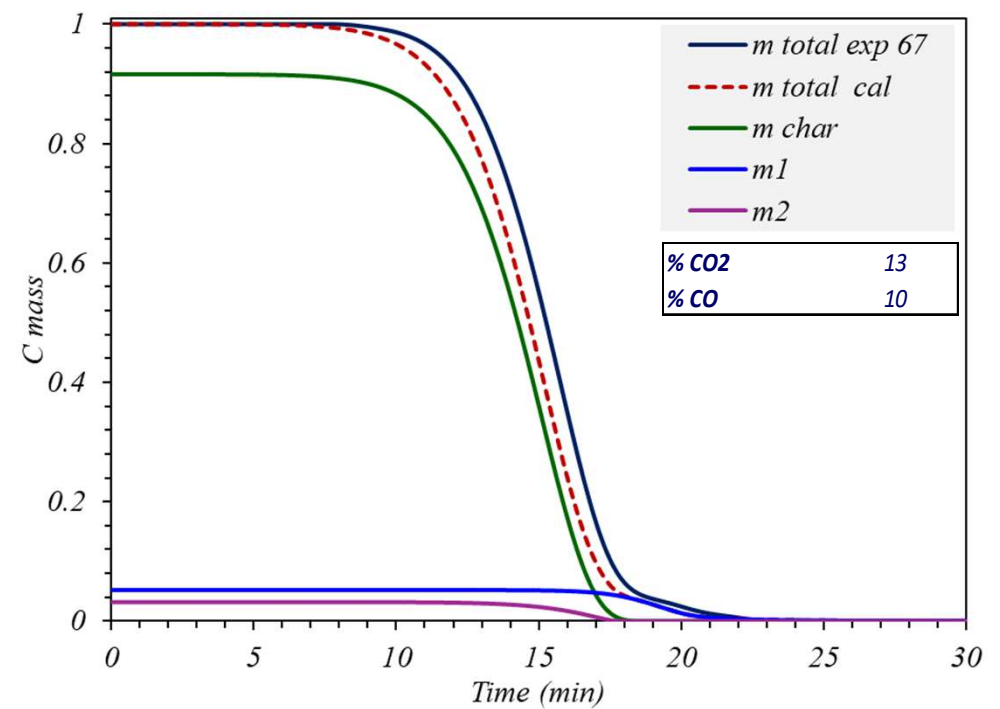
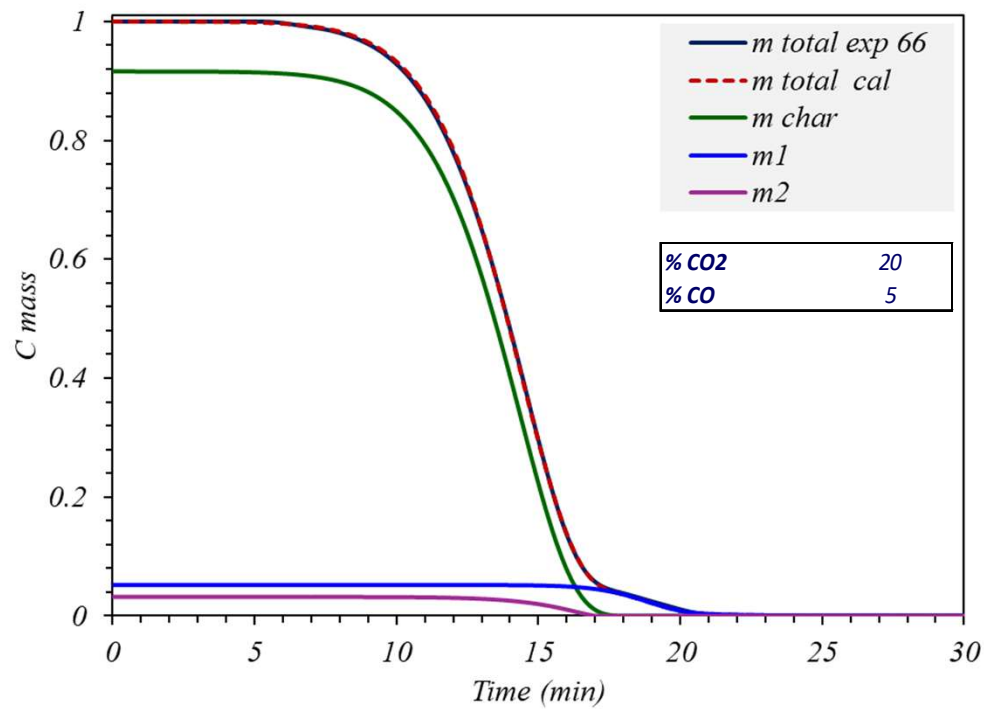
Parallel Kinetic Model - IPR

<i>CO/CO2</i>	<i>0.25</i>	<i>0.77</i>
<i>% CO2</i>	<i>20</i>	<i>13</i>
<i>% CO</i>	<i>5</i>	<i>10</i>
	<i>Exp 66</i>	<i>Exp 67</i>
<i>k char_m (min-1)=</i>	<i>106.9206615</i>	<i>106.9206615</i>
<i>E_char (kJ/mol)=</i>	<i>130.0912659</i>	<i>130.0912659</i>
<i>K_CO2_m (min-1)=</i>	<i>135.1544088</i>	<i>135.1544088</i>
<i>Q_CO2 (kJ/mol)=</i>	<i>140.1691242</i>	<i>140.1691242</i>
<i>K_CO char_m (min-1)=</i>	<i>95.37122132</i>	<i>95.37122132</i>
<i>Q_CO (kJ/mol)=</i>	<i>322.5874739</i>	<i>322.5874739</i>
<i>n char=</i>	<i>0.85943091</i>	<i>0.85943091</i>
<i>m0 char=</i>	<i>0.916043372</i>	<i>0.916043372</i>
<i>k 1_m (min-1)=</i>	<i>0.359596961</i>	<i>0.359596961</i>
<i>E 1 (kJ/mol)=</i>	<i>726.6695001</i>	<i>726.6695001</i>
<i>n 1=</i>	<i>1.521120641</i>	<i>1.521120641</i>
<i>m0 1=</i>	<i>0.052022348</i>	<i>0.052022348</i>
<i>k 2_m (min-1)=</i>	<i>0.14815184</i>	<i>0.14815184</i>
<i>E 2 (kJ/mol)=</i>	<i>446.2684654</i>	<i>446.2684654</i>
<i>n 2=</i>	<i>0.403818805</i>	<i>0.403818805</i>
<i>m02=</i>	<i>0.03193428</i>	<i>0.03193428</i>

	<i>0.25</i>	<i>0.77</i>
	<i>20</i>	<i>13</i>
	<i>5</i>	<i>10</i>
	<i>Exp 66</i>	<i>Exp 67</i>
	<i>M.H.</i>	<i>M.H.</i>
<i>average value</i>	<i>0.055192061</i>	<i>0.051731887</i>
<i>SST</i>	<i>10.47668399</i>	<i>12.15457073</i>
<i>SSE</i>	<i>0.006585226</i>	<i>0.634209572</i>
<i>SSRE</i>	<i>5.77724E+16</i>	<i>8.56668E+16</i>
<i>R2</i>	<i>0.999436102</i>	<i>0.966940756</i>
<i>M.H. (SSE,SSRE)</i>	<i>0.013170451</i>	<i>1.268419145</i>
<i>MSC</i>	<i>8.335104291</i>	<i>3.615562287</i>
<i>MIC</i>	<i>13.25063241</i>	<i>8.609395629</i>
<i>SDE</i>	<i>0.001902457</i>	<i>0.019845893</i>

MSC > 4.5

Parallel Kinetic Model – m C gasified



MSC 8.335104291 3.615562287

Next Steps and Conclusions

- Isothermal Experiments with High CO₂ concentration and Dyn/Iso with High CO₂ + N₂ experiments;
- Feed the kinetic model with experimental data to investigate the effects of Oxy-combustion on the reactivity of the black liquor char.
- The experimental results are still providing fundamental insights into black liquor char gasification and reactivity under oxy-combustion relevant conditions.
- The findings will help to better understand how temperature, CO₂ and CO affect gasification kinetics and char conversion behavior.
- The data will serve as a reliable basis for a development of a kinetic models in CFD simulations.
- Ultimately, these models could support the quantitative prediction of black liquor combustion in kraft recovery boilers operated under oxy-combustion, contributing to process optimization and decarbonization strategies.



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